# Wiring American Flyer Sectional Track

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http://doerry.org/norbert/train/AFtrain.htm



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## 1. Introduction

There are many options for routing wire between a transformer and American Flyer sectional track. This document evaluates the impact of wire gauge (AWG) number of connections, and routing of wires to a notional loop consisting of 40 sections of American Flyer sectional track: 12 curve and 28 straight. Seven different cases are examined for six different gauges of wire and 3 different values of track resistance.

In comparing the options, the following metrics were considered:

- 1. The difference between the highest and lowest resistance of points on the track as measured from the transformer terminal. This difference reflects the variability in speed the engine will experience as it completes a revolution of the track. Experiments conducted on my layout (using a 12B transformer) indicate a difference of 0.5 ohms is barely noticeable at low speeds, but not at high speeds. Allocating half of this resistance difference to each of the two conductors / rails, desirable performance is for each conductor / rail to have a resistance difference of no more than 0.25 ohms. Marginal performance is attributed to a resistance difference greater than 0.5 ohms. Undesirable performance is attributed to a resistance difference greater than 0.5 ohms.
- 2. The average resistance from the sample points to the transformer terminal is not an issue unless it becomes so large that the train engine cannot achieve a reasonable speed when the transformer is at its maximum setting. Subjectively, I determined that the average resistance for each conductor / rail would have to exceed about 0.75 ohms with my 12B transformer before becoming excessive. This only occurs for Case 1, hence average resistance was not used as a discriminator.
- 3. While cost is always of concern, none of the cases used more than 100 ft, and the cost difference between 100 feet of the smallest (22 AWG) and largest (12 AWG) wire is only on the order of \$8 if speaker wire is used. See Table 1 for details.

AWG	length	single conductor stranded	Source	Speaker Wire	Source	ROMEX house wiring	Source
22 AWG	100 ft	\$9.95	Jameco	\$10.95	Audiopipe - Amazon		
20 AWG	100 ft	\$12.95	Jameco	\$11.95	Audiopipe - Amazon		
18 AWG	100 ft	\$18.95	Jameco	\$12.95	Audiopipe - Amazon		
16AWG	100 ft	\$20.95	Jameco	\$14.95	Audiopipe - Amazon		
14AWG	100 ft			\$16.89	Audiopipe - Amazon	\$31.57	Home Depot
12AWG	100 ft			\$18.95	Audiopipe - Amazon	\$48.57	Home Depot

Table 1: Cost of Cable (as of March 29, 2020)

Three different values of track resistance are used because one of the critical factors for track resistance is the degree that the track connectors make good electrical contact. I connected together ten pieces of American Flyer section track without making any special effort to establish a good electrical connection. The resistance of one rail was 0.75 ohms while the other was 1.61 ohms. Based on these measurements, I selected three values of track resistance per section to use in this analysis: 0.025 ohms, 0.075 ohms, and 0.15 ohms. The lower value (0.025 ohms) reflects a value that should be attainable with careful attention to establishing a good electrical connection. The middle value (0.075 ohms) reflects a value attainable with a reasonable effort to establish a good electrical connection, or that value that may happen as the electrical conductivity degrades over time. The higher value (0.15 ohms) reflects a value where little attention has been paid to establishing good electrical conductivity, or where the electrical conductivity has degraded over time.

A desirable configuration achieves the desirable resistance difference for the middle value of track resistance. A highly desirable configuration achieves the desirable resistance difference for the higher value of track resistance.

The resistance per foot of copper wire is listed in Table 2. The source for this data is ASTM B8 and is applicable for 20° C (68° F) which is a reasonable room temperature for a train layout.

Table 2: Resistance (ohms) per foot of stranded copper wire

12 AWG	14 AWG	16AWG	18AWG	20AWG	22AWG
0.00163	0.00258	0.0041	0.00654	0.0103	0.0164

The voltage drop experienced by an engine will be equal to its current draw (amps) multiplied by twice the resistance of a single rail / wire from the point on the track back to the transformer. The American Flyer Service Manual indicates for steam engines, the maximum current draw at 12 volts a.c. can range from 1.75 to 2.3 amps when pulling 4 box cars. For diesels, the maximum current draw can range from 1.8 to 3.25 amps. For post war American Flyer steam engines, the maximum currents I measured on my collection of engines are between 1.6 and 2.5 amps when pulling 8 freight cars (6 gondolas, 1 box car, 1 TOFC). For a dual motor ALCO, I measured a maximum of 2.5 amps. An American Models Baldwin diesel with a can motor had a maximum current draw of 0.6 amps.

Based on the above, one can probably plan on a maximum current of about 2.5 amps. With a maximum track resistance difference of 0.25 ohms for desirable operation, this translates into a maximum voltage variation of  $2 \times 0.25 \times 2.5 = 1.25$  volts.

## 2. Cases

Figures 1 through 7 depict the seven cases and the resistances for three wire gauges and the three track resistances as calculated at points that are near the local maximum and minimum resistance values. The "Delta R" table provides the differences between the maximum and minimum resistances. Combinations of wire gauge and track resistance that resulted in a desirable "Delta R" of 0.25 ohms or less are highlighted in green. Marginal performance is highlighted in yellow, and Undesirable performance is highlighted in orange.

The data for all six wire gauges are presented in Appendix A.

For cases 1 through 6, the track oval was broken into 8 groups of 5 sections of track. The boundaries between groups are nodes labeled: 10, 12, 20, 23, 30, 34, 40, and 41. The transformer terminal is assigned node 0. Each group of tracks was modeled as a resistor with a label beginning with "RT\_" and ending with the labels of the two nodes at its end. In case 7, two of the groups are broken into two subgroups with node 60 midway between nodes 10 and 12, and node 61 midway between nodes 12 and 23. In this case, RT\_1060 and RT\_6012 replace RT\_1012, while RT\_1261 and RT\_6120 replace RT\_1220. The resistances of each track group (including low, medium, and high values) are presented in Table 3.

sections Resistance (ohms) M Н RT 1012 0.75 0.125 0.375 5 RT\_1220 5 0.125 0.375 0.75 RT 2023 5 0.125 0.375 0.75 RT\_2330 5 0.125 0.375 0.75 RT\_3034 5 0.375 0.125 0.75 RT\_3440 5 0.125 0.375 0.75 RT\_4041 5 0.125 0.375 0.75 RT\_4110 5 0.125 0.375 0.75 RT\_1060 2.5 0.0625 0.1875 0.375 RT 6012 2.5 0.0625 0.1875 0.375 RT 1261 0.0625 0.1875 2.5 0.375 RT 6120 0.0625 0.1875 0.375

Table 3: Track group resistance

Copper wires are labeled with "RC\_" followed by the labels of the nodes they connect. Cases 6 and 7 have an additional node 50 used to connect wires together, but not associated with a track group. Details on all of the wires defined in all seven cases are provided in Table 4. All the wires are not used in any one case. Table 5 indicates which wires (cables) are used in each case and the total length of cable required.

Table 4: Resistance of copper wires (ohms)

Wire	length (in)	12 AWG	14 AWG	16AWG	18AWG	20AWG	22AWG
RC_0010	32	0.0043	0.0069	0.0109	0.0174	0.0275	0.0437
RC_1030	154	0.0209	0.0331	0.0526	0.0839	0.1322	0.2105
RC_1020	110	0.0149	0.0237	0.0376	0.0600	0.0944	0.1503
RC_2030	110	0.0149	0.0237	0.0376	0.0600	0.0944	0.1503
RC_3040	110	0.0149	0.0237	0.0376	0.0600	0.0944	0.1503
RC_4010	110	0.0149	0.0237	0.0376	0.0600	0.0944	0.1503
RC_0020	134	0.0182	0.0288	0.0458	0.0730	0.1150	0.1831
RC_0030	180	0.0245	0.0387	0.0615	0.0981	0.1545	0.2460
RC_0040	110	0.0149	0.0237	0.0376	0.0600	0.0944	0.1503
RC_0050	110	0.0149	0.0237	0.0376	0.0600	0.0944	0.1503
RC_1050	80	0.0109	0.0172	0.0273	0.0436	0.0687	0.1093
RC_2050	80	0.0109	0.0172	0.0273	0.0436	0.0687	0.1093
RC_3050	80	0.0109	0.0172	0.0273	0.0436	0.0687	0.1093
RC_4050	80	0.0109	0.0172	0.0273	0.0436	0.0687	0.1093
RC_1250	80	0.0109	0.0172	0.0273	0.0436	0.0687	0.1093
RC_2350	80	0.0109	0.0172	0.0273	0.0436	0.0687	0.1093
RC_3450	80	0.0109	0.0172	0.0273	0.0436	0.0687	0.1093
RC_4150	80	0.0109	0.0172	0.0273	0.0436	0.0687	0.1093

Table 5: Cable lengths and association with cases

			Ca	ble (inche	s)		
	Case 1	Case 2	Case 3	Case 4	Case 5	Case 6	Case 7
RC_0010	32	32	32	32	32		
RC_1030		154					
RC_1020			110	110			
RC_2030			110	110			
RC_3040			110	110			
RC_4010				110			
RC_0020					134		
RC_0030					180		
RC_0040					110		
RC_0050						110	110
RC_1050						80	80
RC_2050						80	80
RC_3050						80	80
RC_4050						80	80
RC_1250							80
RC_2350							80
RC_3450							80
RC_4150							80
			Total	Cable (inc	hes)		
	Case 1	Case 2	Case 3	Case 4	Case 5	Case 6	Case 7
	32	186	362	472	456	430	750

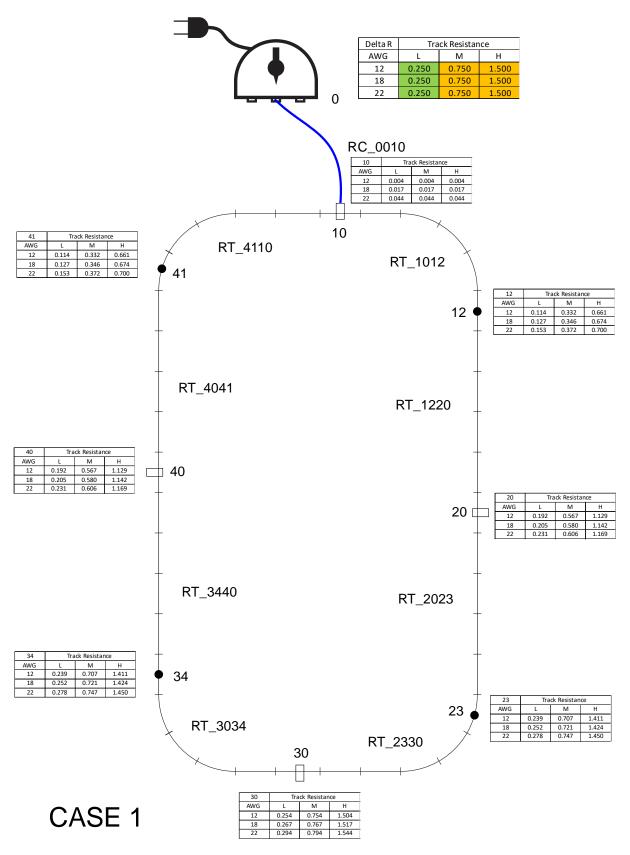


Figure 1: Case 1

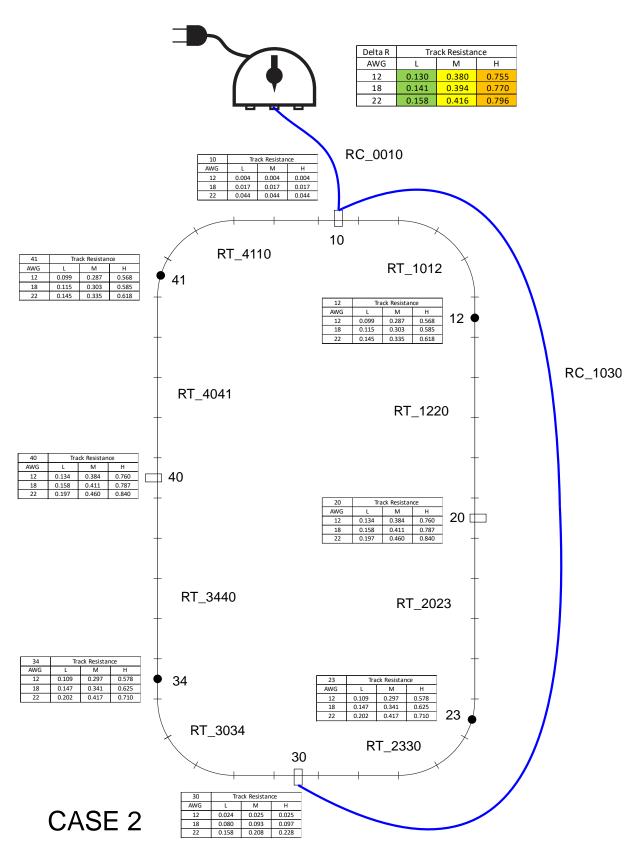


Figure 2: Case 2

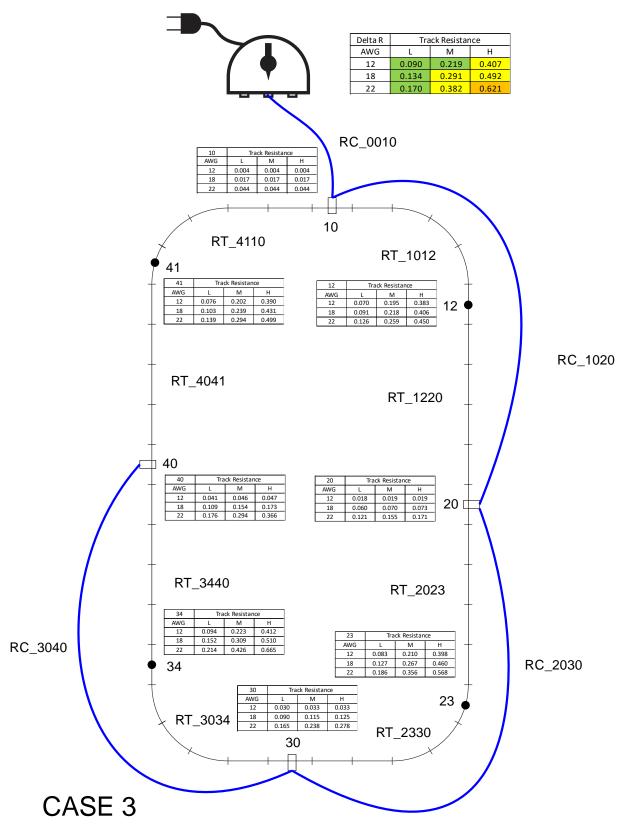


Figure 3: Case 3

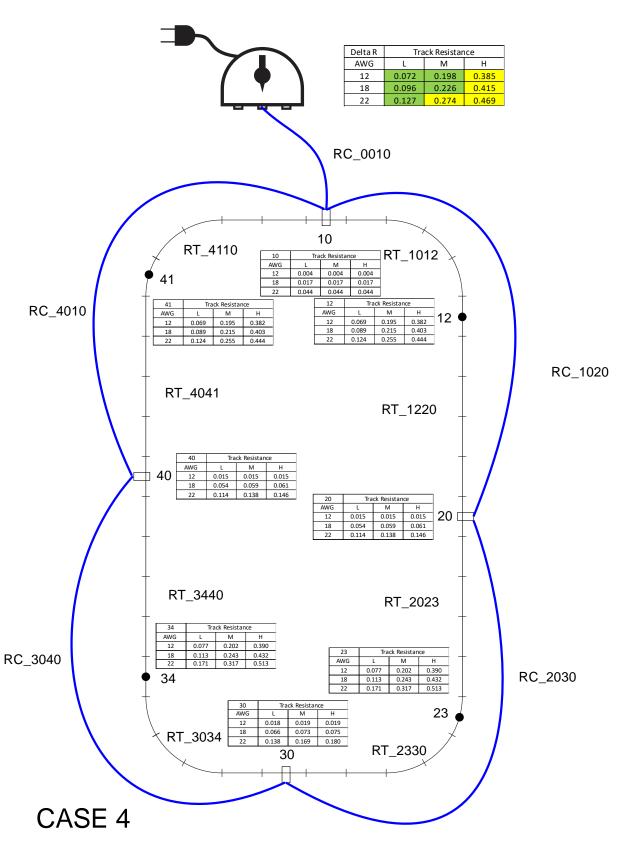
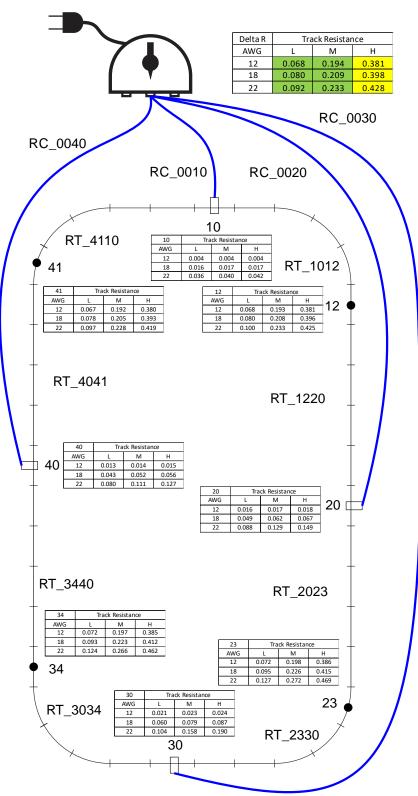


Figure 4: Case 4



CASE 5

Figure 5: Case 5

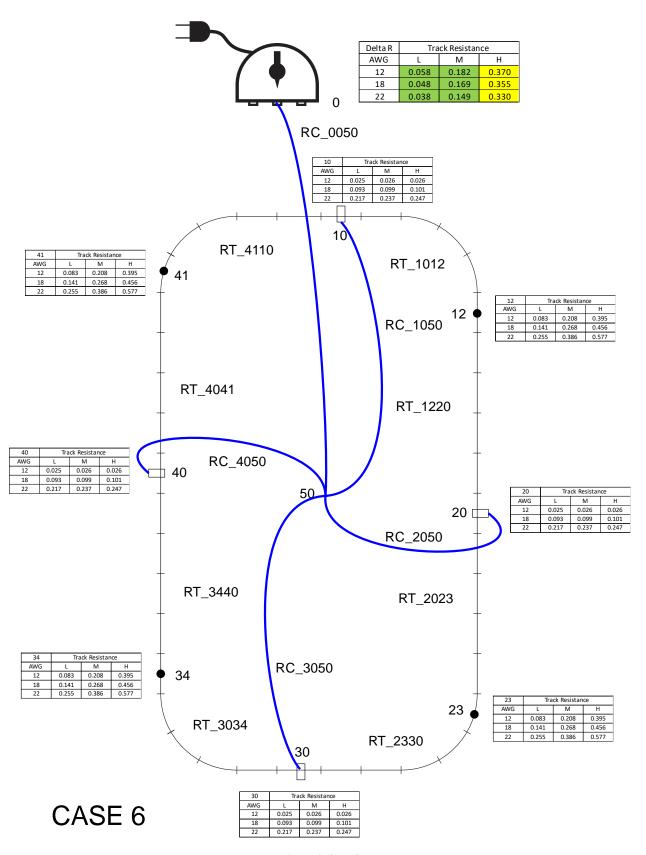
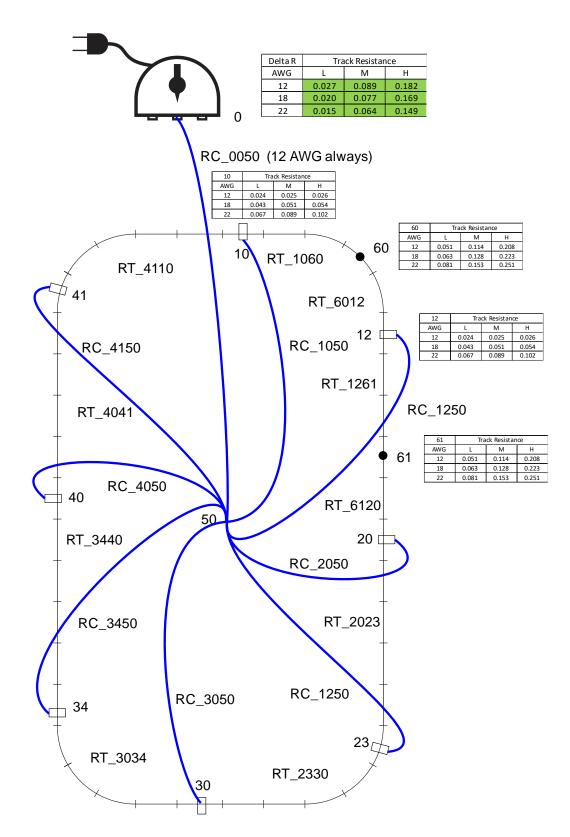


Figure 6: Case 6



CASE 7

Figure 7: Case 7

## 3. Observations and Recommendations

In examining the "Delta R" tables for all seven cases it is apparent that minimizing track resistance has a greater impact on acceptability than increasing the size (lower AWG) of the copper wire. Similarly, adding more connections to the track (1 for Case 1, 2 for Case 2, 4 for Cases 3-6, and 8 for Case 7) has a greater impact than increasing copper wire size. In fact in Case 7, acceptable performance is achieved with the smallest wire (22 AWG).

Based on the results of this analysis, I recommend using a "star" type wiring configuration as depicted in Cases 6 and 7. Key to minimizing the "Delta R" is keeping all of the wires from the common distribution point to the track roughly the same length and the same gauge as well as having track-wire connections no more than 5 track sections apart (as in Case 7). Although of lesser importance, I recommend using 18 AWG wire or larger to reduce the average resistance.

To make it easier to maintain the layout while maintaining a good electrical connection between the wire and track, I recommend soldering the wire directly to the underside of each rail. I recommend soldering about a 9 inch length of 22 AWG wire to the rail. While one would still likely need a high wattage soldering iron (40 watts or more) or a soldering gun, it is easier to solder a 22 AWG wire to a rail than a wire of greater size. Make sure the solder joint area on the track is clean and corrosion free.

Underneath the train table, you can connect the 22 AWG wire to a larger gauge wire using a 2 pole European style terminal block as depicted in Figure 8. The European style terminal blocks usually are purchased with 8 or more poles; but they are easily cut down to size.

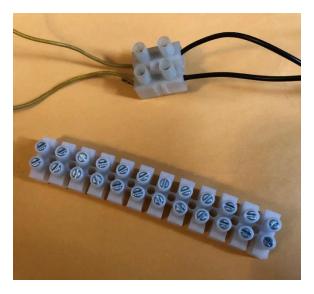


Figure 8: European Style Terminal Blocks

There are many options for the common distribution point. I generally recommend using either the European style Terminal Blocks or a feed through Terminal Block as depicted in Figure 9. You can use one terminal block for each of the two rails. With the feed through Terminal Block, all the terminals can be electrically connected by soldering a bare solid copper wire across all the terminal pole leads; the track and transformer wire are attached using the screws on top. For the European style Terminal Block, you can use solid wire to connect all the terminal poles on one side and connect the track and transformer wire on the other side. There are many other possible solutions that will work just as well.



Figure 9: Terminal Block Examples

## **Appendix A: Data**

		Delta R	0.250	0.250	0.250	0.250	0.250	0.250	0.750	0.750	0.750	0.750	0.750	0.750	1.500	1.500	1.500	1.500	1.500	1.500	0.130	0.132	0.136	0.141	0.147	0.158	0.380	0.383	0.387	0.394	0.403	0.416	0.755	0.758	0.763	0.770
	Smallest	æ	0.004	0.007	0.011	0.017	0.027	0.044	0.004	0.007	0.011	0.017	0.027	0.044	0.004	0.007	0.011	0.017	0.027	0.044	0.004	0.007	0.011	0.017	0.027	0.044	0.004	0.007	0.011	0.017	0.027	0.044	0.004	0.007	0.011	0.017
	Greatest	œ	0.254	0.257	0.261	0.267	0.277	0.294	0.754	0.757	0.761	0.767	0.777	0.794	1.504	1.507	1.511	1.517	1.527	1.544	0.134	0.139	0.147	0.158	0.174	0.202	0.384	0.390	0.398	0.411	0.431	0.460	0.760	0.765	0.774	0.787
	Std	Deviation	0.086	980.0	0.086	0.086	0.086	980.0	0.257	0.257	0.257	0.257	0.257	0.257	0.513	0.513	0.513	0.513	0.513	0.513	0.049	0.048	0.048	0.048	0.050	0.054	0.148	0.148	0.146	0.145	0.144	0.144	0.299	0.298	0.296	0.294
		Average R	0.168	0.171	0.175	0.182	0.192	0.208	0.497	0.499	0.503	0.510	0.520	0.536	0.989	0.991	0.995	1.002	1.012	1.028	0.089	0.095	0.104	0.117	0.135	0.161	0.246	0.252	0.262	0.278	0.300	0.335	0.480	0.487	0.497	0.514
		41	0.114	0.116	0.120	0.127	0.137	0.153	0.332	0.335	0.339	0.346	0.356	0.372	0.661	0.663	0.667	0.674	0.684	0.700	0.099	0.102	0.107	0.115	0.127	0.145	0.287	0.290	0.295	0.303	0.316	0.335	0.568	0.571	0.577	0.585
		40	0.192	0.194	0.198	0.205	0.215	0.231	0.567	0.569	0.573	0.580	0.590	909.0	1.129	1.132	1.136	1.142	1.152	1.169	0.134	0.139	0.147	0.158	0.174	0.197	0.384	0.390	0.398	0.411	0.431	0.460	0.760	0.765	0.774	0.787
from Node		34	0.239	0.241	0.245	0.252	0.262	0.278	0.707	0.710	0.714	0.721	0.731	0.747	1.411	1.413	1.417	1.424	1.434	1.450	0.109	0.117	0.129	0.147	0.170	0.202	0.297	908.0	0.320	0.341	0.372	0.417	0.578	0.588	0.602	0.625
Resistance to transformer (ohms) from Node		30	0.254	0.257	0.261	0.267	0.277	0.294	0.754	0.757	0.761	0.767	0.777	0.794	1.504	1.507	1.511	1.517	1.527	1.544	0.024	0.036	0.054	0.080	0.114	0.158	0.025	0.039	0.060	0.093	0.140	0.208	0.025	0.039	0.062	0.097
o transforn		23	0.239	0.241	0.245	0.252	0.262	0.278	0.707	0.710	0.714	0.721	0.731	0.747	1.411	1.413	1.417	1.424	1.434	1.450	0.109	0.117	0.129	0.147	0.170	0.202	0.297	908.0	0.320	0.341	0.372	0.417	0.578	0.588	0.602	0.625
esistance t		20	0.192	0.194	0.198	0.205	0.215	0.231	0.567	0.569	0.573	0.580	0.590	909.0	1.129	1.132	1.136	1.142	1.152	1.169	0.134	0.139	0.147	0.158	0.174	0.197	0.384	0.390	0.398	0.411	0.431	0.460	0.760	0.765	0.774	0.787
_		12	0.114	0.116	0.120	0.127	0.137	0.153	0.332	0.335	0.339	0.346	0.356	0.372	0.661	0.663	0.667	0.674	0.684	0.700	0.099	0.102	0.107	0.115	0.127	0.145	0.287	0.290	0.295	0.303	0.316	0.335	0.568	0.571	0.577	0.585
		10	0.004	0.007	0.011	0.017	0.027	0.044	0.004	0.007	0.011	0.017	0.027	0.044	0.004	0.007	0.011	0.017	0.027	0.044	0.004	0.007	0.011	0.017	0.027	0.044	0.004	0.007	0.011	0.017	0.027	0.044	0.004	0.007	0.011	0.017
		AWG	12	14	16	18	20	22	12	14	16	18	20	22	12	14	16	18	20	22	12	14	16	18	20	22	12	14	16	18	20	22	12	14	16	18
		Track R	0.025	0.025	0.025	0.025	0.025	0.025	0.075	0.075	0.075	0.075	0.075	0.075	0.15	0.15	0.15	0.15	0.15	0.15	0.025	0.025	0.025	0.025	0.025	0.025	0.075	0.075	0.075	0.075	0.075	0.075	0.15	0.15	0.15	0.15
		CASE	1	1	1	1	1	1	П	1	1	П	1	1	1	1	1	1	П	1	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2

	Delta R	0.780	0.796	0.000	0.102	0.117	0.134	0.152	0.170	0.219	0.235	0.259	0.291	0.332	0.382	0.407	0.425	0.452	0.492	0.547	0.621	0.072	0.077	0.085	960.0	0.110	0.127	0.198	0.203	0.212	0.226	0.245	0.274	0.385	0.391
Smallest	œ	0.027	0.044	0.004	0.007	0.011	0.017	0.027	0.044	0.004	0.007	0.011	0.017	0.027	0.044	0.004	0.007	0.011	0.017	0.027	0.044	0.004	0.007	0.011	0.017	0.027	0.044	0.004	0.007	0.011	0.017	0.027	0.044	0.004	0.007
Greatest	œ	0.808	0.840	0.094	0.109	0.128	0.152	0.180	0.214	0.223	0.242	0.270	0.309	0.360	0.426	0.412	0.432	0.463	0.510	0.574	0.665	0.077	0.084	960.0	0.113	0.137	0.171	0.202	0.210	0.223	0.243	0.273	0.317	0.390	0.398
Std	Deviation	0.291	0.289	0.033	0.034	0.037	0.041	0.046	0.052	860.0	0.098	0.099	0.102	0.108	0.118	0.198	0.197	0.197	0.197	0.200	0.208	0.032	0.032	0.032	0.033	0.035	0.040	660.0	860.0	0.097	0.097	960.0	0.098	0.199	0.198
	werage R [	0.538	0.576	0.052	0.062	0.075	0.094	0.116	0.146	0.116	0.129	0.147	0.174	0.209	0.258	0.211	0.224	0.244	0.274	0.318	0.380	0.043	0.050	090.0	0.074	0.095	0.125	0.106	0.113	0.124	0.141	0.166	0.204	0.200	0.207
	41 /	0.598	0.618	9/0.0	0.082	0.091	0.103	0.118	0.139	0.202	0.210	0.222	0.239	0.262	0.294	0.390	0.399	0.412	0.431	0.459	0.499	690.0	0.073	0.080	0.089	0.103	0.124	0.195	0.199	0.205	0.215	0.231	0.255	0.382	0.386
	40	808.0	0.840	0.041	0.058	0.081	0.109	0.140	0.176	0.046	0.070	0.105	0.154	0.216	0.294	0.047	0.074	0.113	0.173	0.254	0.366	0.015	0.023	0.035	0.054	0.079	0.114	0.015	0.024	0.038	0.059	0.090	0.138	0.015	0.024
	34	0.658	0.710	0.094	0.109	0.128	0.152	0.180	0.214	0.223	0.242	0.270	0.309	0.360	0.426	0.412	0.432	0.463	0.510	0.574	0.665	0.077	0.084	960.0	0.113	0.137	0.171	0.202	0.210	0.223	0.243	0.273	0.317	0.390	0.398
	30	0.149	0.228	0.030	0.044	0.064	0.000	0.123	0.165	0.033	0.050	0.077	0.115	0.167	0.238	0.033	0.052	0.081	0.125	0.187	0.278	0.018	0.028	0.044	990.0	960.0	0.138	0.019	0.030	0.047	0.073	0.111	0.169	0.019	0.030
	23	0.658	0.710	0.083	0.093	0.107	0.127	0.152	0.186	0.210	0.222	0.240	0.267	0.304	0.356	0.398	0.410	0.430	0.460	0.503	0.568	0.077	0.084	960.0	0.113	0.137	0.171	0.202	0.210	0.223	0.243	0.273	0.317	0.390	0.398
	20	0.808	0.840	0.018	0.027	0.041	0.060	0.086	0.121	0.019	0.029	0.045	0.070	0.104	0.155	0.019	0.030	0.047	0.073	0.112	0.171	0.015	0.023	0.035	0.054	0.079	0.114	0.015	0.024	0.038	0.059	0.000	0.138	0.015	0.024
	12	0.598	0.618	0.000	0.074	0.081	0.091	0.105	0.126	0.195	0.200	0.207	0.218	0.234	0.259	0.383	0.388	0.395	0.406	0.424	0.450	690.0	0.073	0.080	0.089	0.103	0.124	0.195	0.199	0.205	0.215	0.231	0.255	0.382	0.386
	10	0.027	0.044	0.004	0.007	0.011	0.017	0.027	0.044	0.004	0.007	0.011	0.017	0.027	0.044	0.004	0.007	0.011	0.017	0.027	0.044	0.004	0.007	0.011	0.017	0.027	0.044	0.004	0.007	0.011	0.017	0.027	0.044	0.004	0.007
	AWG	20	22	12	14	16	18	20	22	12	14	16	18	20	22	12	14	16	18	20	22	12	14	16	18	20	22	12	14	16	18	20	22	12	14
	Track R	0.15	0.15	0.025	0.025	0.025	0.025	0.025	0.025	0.075	0.075	0.075	0.075	0.075	0.075	0.15	0.15	0.15	0.15	0.15	0.15	0.025	0.025	0.025	0.025	0.025	0.025	0.075	0.075	0.075	0.075	0.075	0.075	0.15	0.15
	CASE	2	2	3	3	3	3	3	3	3	3	8	3	8	3	8	3	3	8	3	3	4	4	4	4	4	4	4	4	4	4	4	4	4	4

ច		•	•	•	•	•	۰	۰	•	•	
Std	Deviation	0.197	0.196	0.194	0.192	0.030	0.029	0.028	0.028	0.028	
	Average R	0.218	0.236	0.262	0.304	0.042	0.047	0.054	0.064	0.077	
	41	0.393	0.403	0.419	0.444	0.067	0.069	0.073	0.078	0.086	
	40	0.038	0.061	0.094	0.146	0.013	0.020	0.030	0.043	0.059	
	34	0.411	0.432	0.464	0.513	0.072	9/0.0	0.083	0.093	0.106	
	30	0.048	0.075	0.116	0.180	0.021	0.030	0.043	090.0	0.080	
	23	0.411	0.432	0.464	0.513	0.072	0.077	0.085	0.095	0.109	
	20	0.038	0.061	0.094	0.146	0.016	0.024	0.034	0.049	990.0	
	12	0.393	0.403	0.419	0.444	0.068	0.070	0.074	0.080	0.088	
	10	0.011	0.017	0.027	0.044	0.004	0.007	0.010	0.016	0.024	
	Std Gr	12 20 23 30 34 40 41 Average R D	12 20 23 30 34 40 41 Average R D 0.393 0.038 0.411 0.048 0.411 0.038 0.393 0.218	Std G 12 20 23 30 34 40 41 Average R Deviation 0.393 0.038 0.411 0.048 0.411 0.038 0.393 0.218 0.197 0.403 0.061 0.432 0.075 0.432 0.061 0.403 0.236 0.196	Std G 12 20 23 30 34 40 41 Average R Deviation 0.393 0.038 0.411 0.048 0.411 0.038 0.393 0.218 0.197 0.403 0.061 0.432 0.075 0.432 0.061 0.403 0.236 0.196 0.419 0.094 0.464 0.116 0.464 0.094 0.419 0.262 0.194	Std G 12 20 23 30 34 40 41 Average R Deviation 0.393 0.038 0.411 0.048 0.411 0.038 0.393 0.218 0.197 0.403 0.061 0.432 0.075 0.432 0.061 0.403 0.236 0.196 0.419 0.094 0.464 0.116 0.464 0.094 0.419 0.262 0.194 0.444 0.146 0.513 0.180 0.513 0.146 0.444 0.304 0.192	12         20         23         30         34         40         41         Average R Deviation           0.393         0.038         0.411         0.048         0.411         0.038         0.393         0.218         0.197           0.403         0.061         0.432         0.061         0.403         0.236         0.196           0.419         0.094         0.464         0.116         0.464         0.094         0.419         0.262         0.194           0.444         0.146         0.513         0.186         0.513         0.146         0.192         0.092         0.044         0.304         0.092         0.093         0.093         0.092         0.092         0.093         0.093         0.093         0.093         0.093         0.093         0.093         0.093         0.093         0.093         0.093         0.093 <td< td=""><td>12         20         23         30         34         40         41         Average R D G G G G G G G G G G G G G G G G G G</td><td>12         20         23         30         34         40         41         Average R Deviation           0.393         0.038         0.411         0.048         0.411         0.038         0.393         0.218         0.197           0.403         0.061         0.432         0.061         0.493         0.218         0.197           0.419         0.094         0.464         0.116         0.464         0.094         0.449         0.262         0.196           0.044         0.146         0.513         0.180         0.513         0.146         0.444         0.304         0.192           0.068         0.016         0.072         0.021         0.072         0.013         0.047         0.030           0.070         0.024         0.036         0.046         0.043         0.029         0.047         0.029           0.074         0.034         0.085         0.043         0.083         0.073         0.076         0.029         0.076         0.029</td><td>12         20         23         30         34         40         41         Average R Deviation           0.393         0.038         0.411         0.048         0.411         0.038         0.393         0.218         0.197           0.403         0.061         0.452         0.075         0.432         0.061         0.403         0.236         0.197           0.419         0.094         0.464         0.116         0.464         0.094         0.444         0.364         0.196           0.068         0.016         0.072         0.071         0.072         0.013         0.067         0.042         0.030           0.070         0.024         0.076         0.020         0.069         0.047         0.029           0.074         0.034         0.083         0.030         0.076         0.078         0.028           0.080         0.049         0.093         0.043         0.054         0.028</td><td>_</td></td<>	12         20         23         30         34         40         41         Average R D G G G G G G G G G G G G G G G G G G	12         20         23         30         34         40         41         Average R Deviation           0.393         0.038         0.411         0.048         0.411         0.038         0.393         0.218         0.197           0.403         0.061         0.432         0.061         0.493         0.218         0.197           0.419         0.094         0.464         0.116         0.464         0.094         0.449         0.262         0.196           0.044         0.146         0.513         0.180         0.513         0.146         0.444         0.304         0.192           0.068         0.016         0.072         0.021         0.072         0.013         0.047         0.030           0.070         0.024         0.036         0.046         0.043         0.029         0.047         0.029           0.074         0.034         0.085         0.043         0.083         0.073         0.076         0.029         0.076         0.029	12         20         23         30         34         40         41         Average R Deviation           0.393         0.038         0.411         0.048         0.411         0.038         0.393         0.218         0.197           0.403         0.061         0.452         0.075         0.432         0.061         0.403         0.236         0.197           0.419         0.094         0.464         0.116         0.464         0.094         0.444         0.364         0.196           0.068         0.016         0.072         0.071         0.072         0.013         0.067         0.042         0.030           0.070         0.024         0.076         0.020         0.069         0.047         0.029           0.074         0.034         0.083         0.030         0.076         0.078         0.028           0.080         0.049         0.093         0.043         0.054         0.028	_

AWG 16 18 20 22 12 12 14 16 18

7.74ck R 0.15 0.15 0.15 0.025 0.025 0.025 0.025

Detta R 0.400 0.415 0.436 0.068 0.071 0.075 0.085

Smallest
R
0.011
0.017
0.027
0.044
0.004
0.007
0.016

Greatest
R
0.411
0.432
0.464
0.513
0.072
0.085
0.095

0.092	0.194	0.197	0.202	0.209	0.219	0.233	0.381	0.385	0.390	0.398	0.410	0.428	0.058	0.055	0.052	0.048	0.043	0.038	0.182	0.179	0.175	0.169	0.160	0.149
0.036	0.004	0.007	0.011	0.017	0.026	0.040	0.004	0.007	0.011	0.017	0.027	0.042	0.025	0.039	0.060	0.093	0.142	0.217	0.026	0.040	0.063	0.099	0.153	0.237
0.127	0.198	0.204	0.213	0.226	0.245	0.272	0.386	0.391	0.401	0.415	0.437	0.469	0.083	0.094	0.113	0.141	0.185	0.255	0.208	0.220	0.238	0.268	0.314	0.386
0.029	0.097	0.095	0.092	0.089	0.086	0.083	0.197	0.194	0.191	0.187	0.182	0.175	0.031	0.030	0.028	0.026	0.023	0.020	0.097	960.0	0.094	0.090	980.0	0.080
0.095	0.105	0.111	0.120	0.134	0.153	0.180	0.199	0.205	0.215	0.231	0.253	0.285	0.054	0.067	0.086	0.117	0.164	0.236	0.117	0.130	0.151	0.184	0.233	0.312
0.097	0.192	0.195	0.199	0.205	0.214	0.228	0.380	0.382	0.387	0.393	0.403	0.419	0.083	0.094	0.113	0.141	0.185	0.255	0.208	0.220	0.238	0.268	0.314	0.386
0.080	0.014	0.022	0.034	0.052	0.077	0.111	0.015	0.023	0.036	0.056	0.084	0.127	0.025	0.039	0.060	0.093	0.142	0.217	0.026	0.040	0.063	0.099	0.153	0.237
0.124	0.197	0.202	0.211	0.223	0.241	0.266	0.385	0.390	0.399	0.412	0.432	0.462	0.083	0.094	0.113	0.141	0.185	0.255	0.208	0.220	0.238	0.268	0.314	0.386
0.104	0.023	0.035	0.053	0.079	0.113	0.158	0.024	0.037	0.057	0.087	0.129	0.190	0.025	0.039	090'0	0.093	0.142	0.217	0.026	0.040	0.063	0.099	0.153	0.237
0.127	0.198	0.204	0.213	0.226	0.245	0.272	0.386	0.391	0.401	0.415	0.437	0.469	0.083	0.094	0.113	0.141	0.185	0.255	0.208	0.220	0.238	0.268	0.314	0.386
0.088	0.017	0.027	0.041	0.062	0.000	0.129	0.018	0.028	0.043	0.067	0.100	0.149	0.025	0.039	090'0	0.093	0.142	0.217	0.026	0.040	0.063	0.099	0.153	0.237
0.100	0.193	0.196	0.201	0.208	0.218	0.233	0.381	0.384	0.389	0.396	0.408	0.425	0.083	0.094	0.113	0.141	0.185	0.255	0.208	0.220	0.238	0.268	0.314	0.386
0.036	0.004	0.007	0.011	0.017	0.026	0.040	0.004	0.007	0.011	0.017	0.027	0.042	0.025	0.039	090.0	0.093	0.142	0.217	0.026	0.040	0.063	0.099	0.153	0.237
22	12	14	16	18	20	22	12	14	16	18	20	22	12	14	16	18	20	22	12	14	16	18	20	22
0.025	0.075	0.075	0.075	0.075	0.075	0.075	0.15	0.15	0.15	0.15	0.15	0.15	0.025	0.025	0.025	0.025	0.025	0.025	0.075	0.075	0.075	0.075	0.075	0.075

		Delta R	0.370	0.367	0.362	0.355	0.345	0.330
	Smallest	œ	0.026	0.040	0.064	0.101	0.158	0.247
	Greatest	œ	0.395	0.407	0.426	0.456	0.502	0.577
	Std	Deviation	0.198	0.196	0.194	0.190	0.184	0.176
		Average R	0.210	0.224	0.245	0.279	0.330	0.412
		41	0.395	0.407	0.426	0.456	0.502	0.577
		40	0.026	0.040	0.064	0.101	0.158	0.247
from Node		34	0.395	0.407	0.426	0.456	0.502	0.577
esistance to transformer (ohms) from Node		30	0.026	0.040	0.064	0.101	0.158	0.247
to transforr		23	0.395	0.407	0.426	0.456	0.502	0.577
esistance 1		20	0.026	0.040	0.064	0.101	0.158	0.247
_		12	0.395	0.407	0.426	0.456	0.502	0.577
		10	0.026	0.040	0.064	0.101	0.158	0.247
		AWG	12	14	16	18	20	22
		Track R	0.15	0.15	0.15	0.15	0.15	0.15
		CASE	9	9	9	9	9	9

CASE 7

		Resistano	e to transforr	mer (ohms) fr	om Node					
							Std	Greatest	Smallest	
Track R	AWG	10	60	12	61	Average R	Deviation	R	R	Delta R
0.025	12	0.024	0.051	0.024	0.051	0.038	0.016	0.051	0.024	0.027
0.025	14	0.029	0.054	0.029	0.054	0.041	0.014	0.054	0.029	0.025
0.025	16	0.035	0.058	0.035	0.058	0.046	0.013	0.058	0.035	0.023
0.025	18	0.043	0.063	0.043	0.063	0.053	0.012	0.063	0.043	0.020
0.025	20	0.053	0.071	0.053	0.071	0.062	0.010	0.071	0.053	0.017
0.025	22	0.067	0.081	0.067	0.081	0.074	0.009	0.081	0.067	0.015
0.075	12	0.025	0.114	0.025	0.114	0.070	0.051	0.114	0.025	0.089
0.075	14	0.031	0.117	0.031	0.117	0.074	0.050	0.117	0.031	0.086
0.075	16	0.039	0.121	0.039	0.121	0.080	0.048	0.121	0.039	0.082
0.075	18	0.051	0.128	0.051	0.128	0.090	0.045	0.128	0.051	0.077
0.075	20	0.067	0.138	0.067	0.138	0.103	0.041	0.138	0.067	0.071
0.075	22	0.089	0.153	0.089	0.153	0.121	0.037	0.153	0.089	0.064
0.15	12	0.026	0.208	0.026	0.208	0.117	0.105	0.208	0.026	0.182
0.15	14	0.031	0.211	0.031	0.211	0.121	0.104	0.211	0.031	0.179
0.15	16	0.040	0.216	0.040	0.216	0.128	0.101	0.216	0.040	0.175
0.15	18	0.054	0.223	0.054	0.223	0.139	0.098	0.223	0.054	0.169
0.15	20	0.074	0.234	0.074	0.234	0.154	0.093	0.234	0.074	0.160
0.15	22	0.102	0.251	0.102	0.251	0.176	0.086	0.251	0.102	0.149

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Version 1.3, 3 November 2008

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